



# **Review of alternative measures that minimise mortality of unwanted catch in UK king scallop (*Pecten maximus*) fisheries**

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Version 1.



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## Review of alternative measures that minimise mortality of unwanted catch in UK king scallop (*Pecten maximus*) fisheries

### Executive Summary

The MSC Fisheries Assessment Methodology requires that fisheries adequately consider the MSC Principles & Criteria in relation to gear selectivity. This review summarises;

- the current legal requirements for dredge design for the four nations of the UK and the Isle of Man;
- the research and development, designed to understand and mitigate adverse effects of dredging on scallops and bycatch organisms;
- the various innovations which have been tested, as far as is possible, in terms of their main environmental effects.

The effects of capture in terms of selectivity, damage and stress on scallops and other organisms which the dredge encounters are described. The main findings were:

- That much of the lethal damage to scallops occurs at the first point of contact with the dredge's teeth with the damage rates related to shell strength and varying between grounds.
- Retention in the gear and sorting on deck causes sublethal stress in undersized scallops and the main benefits of selectivity are that this stress is reduced.
- The low efficiency of the dredges means that observations of catch and bycatch of mega-faunal species including scallops landed on the deck only gives a limited indication of levels of damage caused by dredging to these species. More information is available from diver observations post dredging.

The performance of the various gear innovations researched and tested are compared where feasible in the terms of the dredges' impact on the seabed, quantities of scallops retained, level of stress in scallops, quantities of stones retained by the gear, damage to bycatch and fuel efficiency are compared where feasible.

Innovative approaches to dredge design including robotic dredges are reviewed, and the properties of materials available for dredge construction are discussed.

Note that there is ongoing work on understanding the interactions between Endangered, Protected and Threatened (ETP species) and scallop dredging, and this will be reviewed in due course.

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## Table of Contents

Executive Summary .....	3
1 Introduction .....	6
1 UK scallop dredge technical measures .....	8
2 Process and effects of scallop dredging .....	10
2.1 Implications of damage rates and dredge efficiency .....	12
2.2 Effects on king scallop .....	14
2.3 Effects of changes in teeth spacing and design .....	16
2.4 Effects of alternative mechanisms for lifting scallops out of the seabed .....	19
2.5 Effects of changes in dredge belly design.....	22
2.6 Scallop belly ring selectivity.....	23
3 Robotic dredge designs .....	24
4 Materials used in dredge construction.....	25
5 Conclusion; Comparison of dredge designs.....	28
6 References.....	33

## 1 Introduction

The MSC Fisheries Assessment Methodology (MSC, 2019) requires that fisheries adequately consider the MSC Principles & Criteria, in relation to gear selectivity, namely that fisheries should:

**“make use of fishing gear and practices designed to avoid the capture of non-target species (and non-target size, age, and/or sex of the target species); minimise mortality of this catch where it cannot be avoided, and reduce discards of what cannot be released alive”** (Criterion 3B.12).

In addition, FAO (1995), states that;

**“selective and environmentally safe fishing gear and practices should be further developed and applied, to the extent practicable, in order to maintain biodiversity and to conserve the population structure and aquatic ecosystems and protect fish quality. Where proper selective and environmentally safe fishing gear and practices exist, they should be recognized and accorded a priority in establishing conservation and management measures for fisheries.”**

To ensure this, the MSC has recently added a “Review of alternative measures” to several performance indicators to encourage the development and implementation of technologies and operational methods that minimise mortality of unwanted catch or ETP species”, the desired outcomes being:

- To motivate fishers to continually “think smart” about their impact on the environment (species and habitats); both in delivering the sustainable impact most efficiently - and continuing to reduce their impact beyond that.
- To balance this desire with efficiency by not spending a lot of money and time generating only marginal improvements.

To achieve this for species, the scoring issue has been added to the P1 Harvest Strategy (PI 1.2.1) and P2 Species Management PIs (PI 2.1.2, 2.2.2, 2.3.2) requiring fisheries to continually review alternative measures to encourage the development and implementation of technologies and operational methods that minimise mortality of unwanted catch or ETP species, taking into account the practicality of the measures, their potential impact on other species and habitats and on the overall cost of implementing the measures.

Fisheries need to either review alternative measures that are shown to minimise mortality of the species or species group in question. Fisheries also need to consider alternative measures to reduce impacts on habitats. Fisheries should also take account of the potential for both positive and negative impacts of alternative measures on species and habitats when considering whether such measures should be implemented.

Alternative measures should avoid capture of the species in the first place or increase its survivability if released. Alternatively, in the case of in-scope species, they could utilise the unwanted catch in

some way so that it would no longer be 'unwanted'. If there are no unwanted species, the scoring issue on reviewing alternative measures does not need to be scored in that PI.

**Alternative Measures Definition:** Fishing gear and practices that have been shown to minimise the rate of incidental mortality of the species or species type to the lowest achievable levels.

### Alternative Measures Scoring Guideposts

**SG 60** There has been a **review** of the potential effectiveness and practicality of alternative measures to minimise UoA-related mortality of unwanted catch of the target stock/secondary species/ ETP Species.

**SG 80** There is a **regular** review of the potential effectiveness and practicality of alternative measures to minimise UoA-related mortality of unwanted catch of the target stock/secondary species/ ETP Species and they are implemented as appropriate.

**SG 100** There is a **biennial** review of the potential effectiveness and practicality of alternative measures to minimise UoA-related mortality of unwanted catch of the target stock/secondary species/ ETP Species., and they are implemented, as appropriate.

**Table 1** Tabulation of scoring guideposts

Performance indicator and scoring issue	Species group	Comment
1.2.1 Harvest strategy f	Target species	The selectivity parameters of the dredge on the target species scallops are well known. Technical measures are reviewed irregularly by the devolved administrations
2.1.2 Primary species management strategy e	Main species	
2.2.2 Secondary Species management strategy e	Secondary species	Bycatch quantification has been investigated, through scientific studies of bycatch (see below) and analysis of catch from regular dredge surveys in certain locations (Scotland, Isle of Man).
2.3.2 ETP species management strategy e	ETP species	In progress

## 1 UK scallop dredge technical measures

The UK devolved administrations have introduced their own technical measures for scallop dredge tooth spacing and mesh size, partly based on the results of the Ecodredge project (Lart ed. 2003), these are shown in Table 2, together with the regional Minimum Conservation Reference Sizes (MCRS). Table 3 shows the applicable European regulations on Minimum Conservation Reference Size (MCRS) for scallops.

The regulations are expressed in different ways regionally.

- The internal dimension of the ring or tooth spacing is given in millimetres
- The number of rings or teeth across the dredge are used to define the characteristics of the gear taking into account 'turn ups' of one ring at each side of the dredge which are not fixed to the bar.

The latter regulations are designed to enable surveillance to consist of simply measuring total width of the dredges and counting the number of teeth across the bar and rings hanging from the bar

The tooth spacing is expressed as number of teeth per bar in some administrations or as tooth spacing in others. The English, Northern Irish and Isle of Man regulations are all designed to result in 75 mm inside diameter belly rings, with 10 mm diameter wire. The Welsh regulations are designed to result in a ring size of 85 mm with 10 mm wire.



Table 2 Current scallop dredge selectivity measures (2021)

Administration	Measures and effective dimension (>80 cm dredges; the numbers of rings and teeth are adjusted for smaller <80 cm dredges)			Selectivity of belly ring size measure based on Ecodredge results; L <sub>50</sub> <sup>1</sup> See section 2.6	MCRS shell length (mm)	Other measures	Ref
	Teeth Bar length = 705 mm	Rings	Mesh (mm)	Rings (wire=10mm)			
England Outside relevant area	9 teeth/bar if teeth are ≤12 mm width 12mm=75 mm spacing Or 8 teeth/bar if any tooth measures > 12 mm width	8 rings hanging from bar= 75 mm id	No reg	L <sub>50</sub> = 85 mm	100	Must have a spring-loaded tooth bar. No attachments or diving plates. Maximum weight 150 kg. No attachments obstructing the belly rings	The Scallop Fishing (England) Order 2012
England Inside relevant areas which is; Irish Sea N. of 52°30' excluding Scottish waters and all of ICES Division 7d	8/bar 12 mm width spacing = 87 mm	8 rings hanging from bar = 75 mm id.	No reg	L <sub>50</sub> = 85 mm	110		
Wales	8/bar and not more than 22 mm dia. and 110 mm long. Tooth spacing approx. 75-87 mm	7 hanging from bar = 85 mm id	No reg	L <sub>50</sub> = 97 mm	110		
Northern Ireland	75 mm spacing	75 mm id	100	L <sub>50</sub> = 85 mm	110	No French dredges	Conservation of scallops (Northern Ireland) 2008
Isle of Man	75 mm 9 teeth/bar (12 mm teeth)	Clear opening of 75 mm id.	100	L <sub>50</sub> = 85 mm	110	No French dredges	Licence conditions under Isle of Man Sea fishing licence
Scotland	9 teeth/bar if teeth are <12 mm width or 8 teeth/bar if any tooth measures > 12 mm width max tooth length	8 rings hanging from bar= 75 mm id. Same for backs	No reg	L <sub>50</sub> = 85 mm	105	No attachments that obstruct netting or rings French dredges are banned.	The Regulation of Scallop Fishing (Scotland) Orders 2005 and 2017

<sup>1</sup> L<sub>50</sub>= Length at 50% retention rounded to the nearest mm

**Table 3 European Union regulations (REGULATION (EU) 2019/1241)**

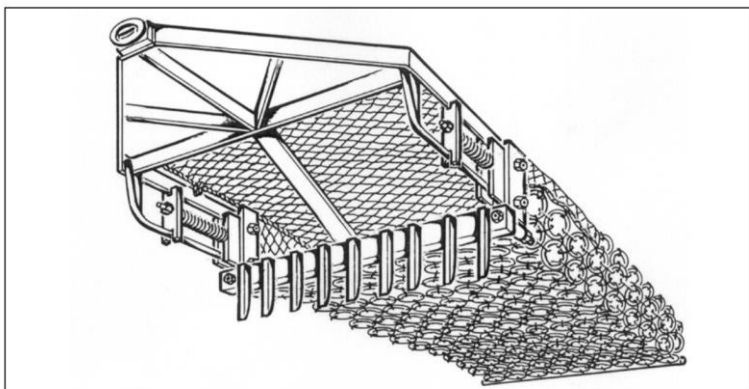
Locations	MCRS (shell length; mm)
All EU waters except below	100
In ICES division 7a (Irish Sea) north of 52° 30' N, and ICES division 7d (Eastern English Channel)	110

Article 8 requires that 95% by live weight of catch consists of bivalve or gastropod molluscs or sponges.

## 2 Process and effects of scallop dredging

Spring toothed (or 'Newhaven') scallop dredges (Figure 1) are towed in gangs of several dredges behind towing bars as shown in Figure 2. Apart from the rubber wheels at the ends of the bars, teeth form the first major penetrative contact with the seabed, and it is the interaction between the teeth and the scallops, which enables the capture of the scallops. The mechanism for capture has been investigated in the Ecodredge<sup>2</sup> project, and a hypothesis of the capture mechanism is based on video camera observations is shown in Figure 3. The mean depth of penetration has been found to be approximately 25 mm on sand-gravel, with deeper penetration 35-59 mm on more gravelly substrates.

Following behind the teeth, the steel ring collector bag the lower part of which is referred to as the dredge belly is towed over the seabed. There is usually a build-up of catch and stones, which substantially increases the weight of the bag (16-78 kg per bag have been estimated, the amount dependent on the amount of stones and catch picked up from the seabed) hence its effect on the seabed and the organisms present increases with the length of the tow. Tensions on the shackles which attaches each dredge frame to the bar have been estimated at 100-180 Kgf. Dredges have been observed to bounce across the seabed apparently mediated by resonance building up in the springs.



**Figure 1 Newhaven 'spring' Scallop dredge**

<sup>2</sup> For full details see Section 3.1.1.1 Ecodredge Investigations Volume 2 (Lart, ed 2003)

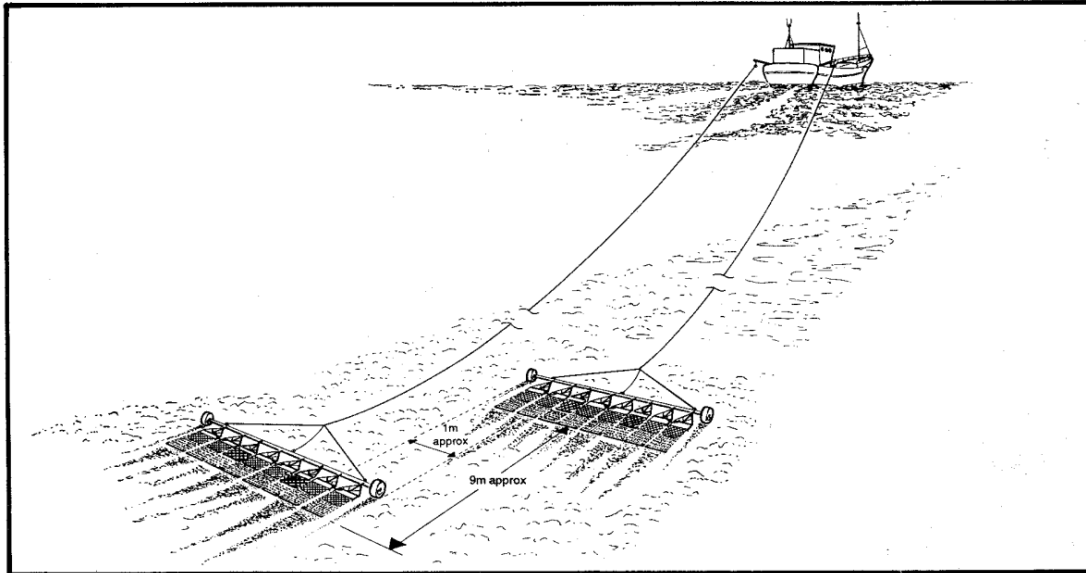


Figure 2 Newhaven ‘Spring’ scallop dredge: Fishing operation. Note, not all vessels use the staggered towing method, some tow with equal length warps from booms positioned forward in the vessel

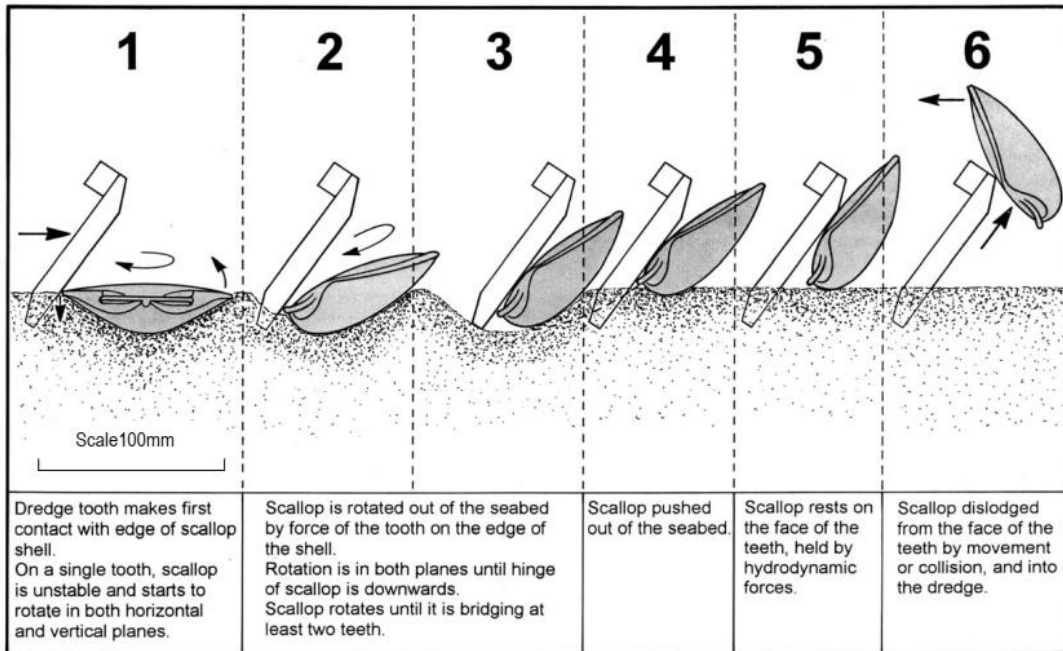


Figure 3 Hypothesised method of scallop capture by spring toothed dredge based upon video observations. Tooth angle set at 55° the mean angle and depth of penetration measured on sandy gravel

## 2.1 Implications of damage rates and dredge efficiency

In order to fully evaluate the effects of scallop dredging on the encountered biota there is a need to study the effects of dredging on both the organisms captured and retained by the gear and those encountering the gear but left on the seafloor. Methods have been developed (Veal et al, 2000) to describe the levels of damage, in terms of damage scores (see **Error! Reference source not found.**), and subsequent survival under laboratory conditions, for a variety of megafauna species. These methods have been used to examine the damage and survival potential of both those specimens captured and retained by the gear and those left in the dredge track (Jenkins et al., 2001).

Key findings were;

- The mean level of damage to a number of common megafaunal species was compared between captured organisms landed on deck (bycatch), and those encountering the dredge but left on the seabed. For many species including scallops, the mean damage rates were similar. For some species such as brown crab (*Cancer pagurus*) damage rates were higher for those specimens left on the seafloor, suggesting that passage under the dredge was more damaging than being retained by the dredge.
- The low level of efficiency of capture by the dredges combined with roughly equivalent levels of damage between the bycatch (ie the catch landed on deck) and animals left on the seabed for most species studied, means that observation of bycatch alone gives only a limited indication of levels of damage to megafauna (see Figure 4).
- Combining the damage rates for those animals left on the seabed and those landed on deck for the mega faunal species enables an overview of the percentage by number of the damage rates of species encountering the gear (Table 4)

Table 4 Predicted level of damage to megafauna in the path of spring toothed scallop dredges (bycatch and non-captured animals combined) as a percentage of individuals with each damage score, from Jenkins et al., (2001). Damage scores are calibrated from 1; no visible damage, through to 3 – 4 lethal damage; see Veale et al., (2001) for a full description of scores.

Species	Damage score			
	1	2	....3	.... 4
<i>Asterias rubens</i>	93.2	6.2	0.4	0.2
<i>Crossaster papposus</i>	92.1	7.6	0.0	0.3
<i>Astropecten irregularis</i>	67.5	26.8	4.6	1.1
<i>Porania pulvillus</i>	99.8	0.2	0.0	0.0
<i>Luidia ciliaris</i>	53.3	38.6	15.3	20.4
<i>Echinus esculentus</i>	53.3	1.1	29.3	16.4
<i>Neptunea antiqua</i>	76.7	23.2	0.1	0.0
<i>Cancer pagurus</i>	36.8	13.9	6.1	43.2
<i>Liocarcinus</i> spp.	50.0	6.1	7.7	36.3
<i>Pecten maximus</i>	93.0	1.8	2.9	2.3

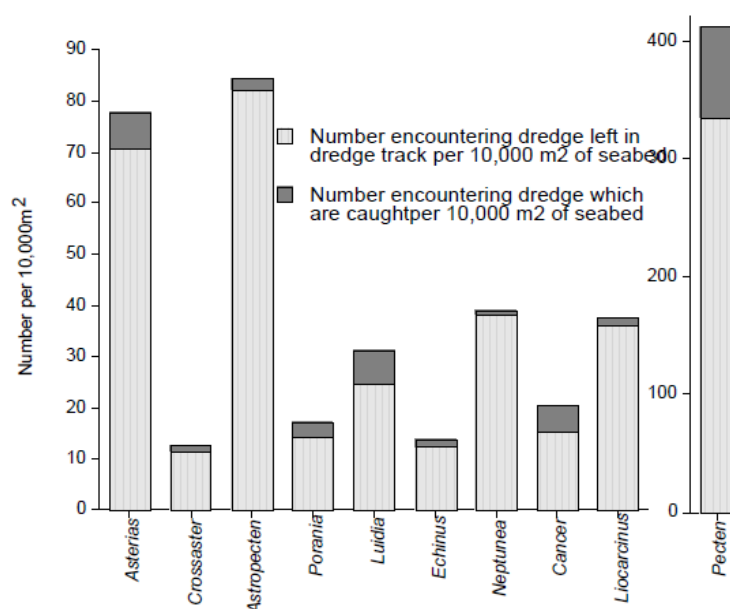


Figure 4 Density (calculated as number per 10,000m<sup>2</sup> of seabed) and efficiency of capture by spring toothed scallop dredges of 10 megafaunal species (Jenkins et al., 2001).

## 2.2 Effects on king scallop

The effects of capture and selection at the dredge and capture followed by selection on deck were examined by the Ecodredge project using field and laboratory studies of the effects of dredging and simulated dredging on scallops. Stress in scallops was estimated using the Adenylate Energy Charge (AEC) levels (see Appendix 1) in the straited adductor muscle which is the muscle that the scallop uses for swimming (Maguire et al., 2002a,b). In essence, this is an index of the immediately available energy which the scallop can use for swimming, jumping and recessing.

Stress was also examined through behavioural observations; the rate at which scallops reburied in the sediment (Maguire et al., 2002a,b) and the behavioural response of the scallops to predators (Jenkins and Brand, 2001). The effects of damage and stress factors on attraction of predators and consequences of predation were investigated using baited cameras (Jenkins et al., 2004).

Key findings were;

- The stress effects as elicited by AEC and behavioural studies in scallops were related to the duration of dredging and severity of the acceleration which the scallops were subjected to during dredging. AEC levels were recovered in between 6 and 24 hours after dredging, but certain aspects of the scallop's behavioural response to predators continued for 24 hours or more.
- The AEC levels in scallops which were collected from the dredge track by divers were found to be similar to those which had undergone simulated dredging for 16 minutes. Scallops which had been towed for 45 minutes within the dredge bag were considerably more stressed (lower AEC levels) than those collected from the dredge track.
- Damage levels of scallops in the catch and recovered from the dredge tracks were not significantly different. Further studies of damage rates and other factors including volumes of stones in the dredges lead to the conclusion that the majority of the damage occurred during initial impact with the dredge teeth (see also Section 4.2). Variation in shell thickness, structure and strength of scallops' shells appeared to be the principle driver for variation in damage levels between scallop fishing grounds (Stewart et al, 2021).

The consequences of damage and stress were examined by observations of scallops placed before cameras in experimental plots (stressed by simulated dredging and application of minor or major shell damage) by Jenkins et al., (2004). Batches of scallops which were undamaged, lightly damaged, and badly damaged were tested:

- Density of scavengers at the stressed but undamaged scallops was equivalent to the density during un-baited periods, which suggests that stressed scallops do not attract scavengers.
- For the damaged scallops there was a significant increase in scavenger density over the study period of 96 hours
- The badly damaged scallops were all eaten within just over 24 hours for each of the 2 replicate periods.
- The scallops that were lightly damaged survived longer, but survival rates differed among replicates.

These results indicate that the mortality of undersized scallops discarded back onto the grounds they were fished on is more likely to be related to shell damage than stress induced by dredging. However, there are two caveats which should be added:

- The predators and scavengers which the scallops were exposed to were markedly different by comparison with those of a previous study, at the same site, four years previously. The previous study found large aggregations of the predatory starfish *Asterias rubens* and *Astropecten irregularis*, and the crabs *Liocarcinus* species and *Pagurus* species. In general, the scavenger community observed in this study differed markedly, with a greater dominance of fish and an increased importance of the edible crab *Cancer pagurus*.
- It is conceivable that the results may have been different had the stressed but lightly or undamaged scallops been exposed to more starfish as in the previous study. It is notable that although the AEC levels of experimentally stressed scallops recovered within 6 to 24 hours, their response to starfish was affected for at least this period in experimental studies (Jenkins and Brand, 2001).



**Figure 5: The N-Virodredge design (left) separate from the steel belly bag, with individually sprung tines and side skids; compared to the Newhaven dredge (right) with a fixed tooth bar. Source: Filippi, (2013).**

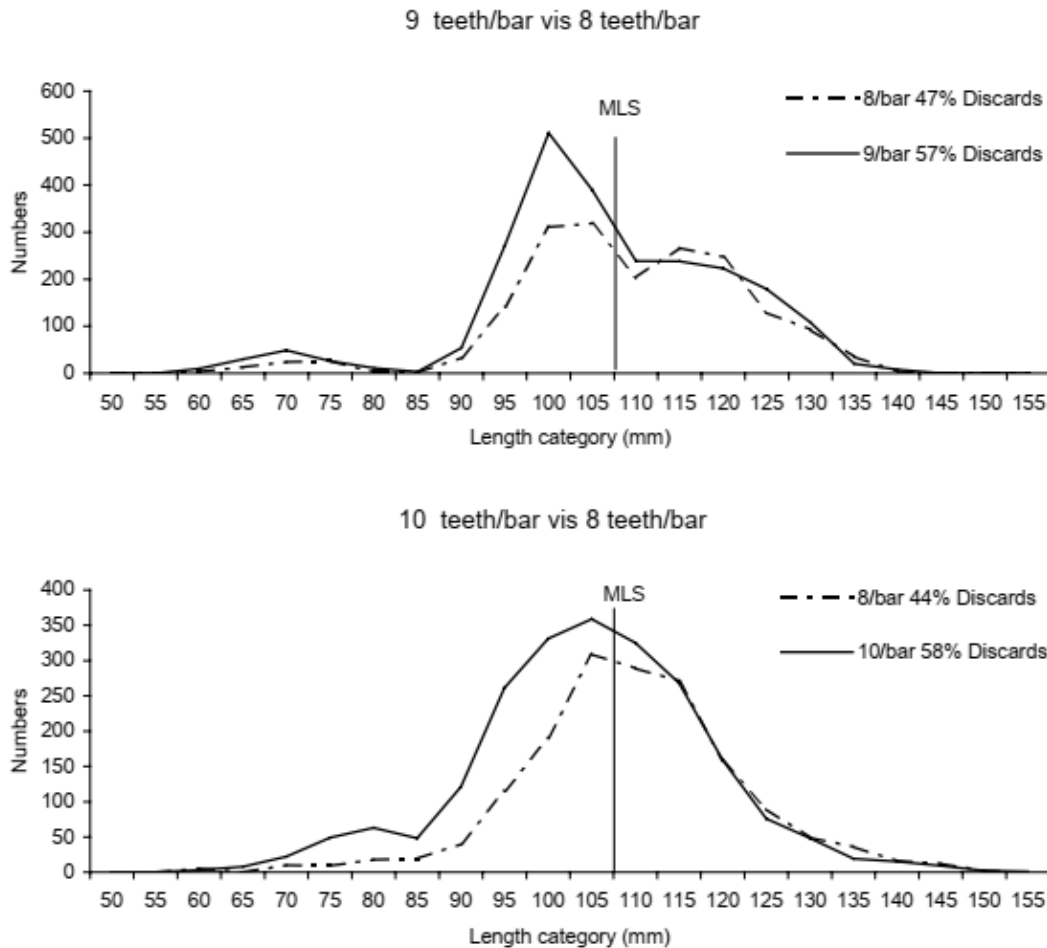
### 2.3 Effects of changes in teeth spacing and design

There is good evidence (see above) that much of the lethal damage to scallops occurs at contact with the teeth, so understanding the effects of tooth design is an important element in understanding measures taken to reduce the effects of dredges.

#### *Teeth spacing*

Minimising the amount of time the scallops spend in contact with the gear will minimise stress on the scallops (see section 2.2). There is evidence that increasing tooth spacing improves selectivity (Figure 6) which happens instantly at the teeth, so regulating tooth spacing is a valid option for controlling selectivity. The experimental results for so called 'French' teeth of 12 mm width consistently showed increasing selectivity with increasing spacing. The English regulations (Table 2) require 8 teeth/bar in areas (North Irish Sea and Eastern Channel) where the MCRS is 110 mm, but 9 teeth/bar elsewhere. The Welsh regulations in Welsh waters require 8 teeth/bar. Evidence for the spacing of the 'peg' teeth of 20 mm diameter influencing the selectivity of the gear is not available.





**Figure 6 Length frequency distributions for catch comparisons between 8, 9, and 10 teeth to the bar for 12 mm wide teeth. Both these plots show evidence of selectivity**

*N-Virodredge*

The N-Virodredge<sup>TM 3</sup> is a modification of the Newhaven dredge designed and patented by Deeside Marine Ltd (Kirkcudbright). The sprung tooth bar is replaced by individually sprung tines around 17 cm long and 8 mm wide. Skids on each end of the tine bar support the weight of the bar (Figure 5). The intention behind this design is to move the weight of the dredge from the teeth on to the side skids, hence reducing the pressure at the teeth, and the design enabling the tines to move independently (Chris Bird pers. comm). Trials in the Bay de Seine (Fillippi, 2013) comparing the N-Virodredge<sup>TM</sup> with spring tooth dredges (although not on the same vessel) over a period of 3 months with 4 vessels showed at least equivalent

<sup>3</sup> <http://n-virodredge.com/>

levels of efficiency and yields, although influenced by seabed composition. The results also indicated;

- A virtual absence of chipped or broken shells and less off size scallops (presumably small scallops) captured
- A reduction in the quantity of stones retained by the gear
- Fuel savings estimated at between 12.2 and 31.4%.

The main operational issues were related to the durability of the teeth, provided the teeth lasted for a minimum of 2 days, the maintenance cost of the dredges was 10% less for the N-Virodredge™ compared with standard spring toothed dredges.

A study reported to [ICES WGScallop \(2015\)](#) in 2015 compared the effects of N-Virodredge™ on with standard spring toothed scallop dredges on sandy and mixed sediments (EUNIS class A5.33 and 5.43; (see (<https://eunis.eea.europa.eu/habitats.jsp>) in Clew Bay on the west coast of Ireland both in terms of bycatch and environmental effects post dredging from diver observations. They report;

- Catch rates for scallops in the N-Virodredge™ were slightly higher than standard spring toothed dredges and with less variability
- Bycatch was similar in both dredges and there was no apparent difference in selectivity
- Sources of physical impact include the rollers at the end of the dredge beam,
  - the dredge teeth or tines (N-Virodredge™) and the weight of the of the dredge
  - bag (chain mat)
- Tracks from both dredges were clearly visible in the days following dredging. However, diver surveys were not able to detect a difference in the impact of the two dredge types
- The N-viro dredge teeth were observed to penetrate the seabed up to their full extent (12-15 cm). However, this may be a reflection of the habitat present (relatively fine sand for scallop dredging) and may not be typical.

#### *Overall effects of damage at teeth*

Lethal and sub lethal damage rates of scallops observed in the catches of standard spring toothed dredges are relatively low; around 2-11%, and related to shell strength which varies between grounds (Stewart et al., 2021). However, the low efficiency of the dredges (Figure 4) means that there are more scallops and other organisms affected by dredging than appear in the catches. Therefore, any reduction in damage as has been reported to be achieved for

with the N-Virodredge™ tooth design (see above) would be beneficial to reducing the effects of dredging on non-retained scallops

## 2.4 Effects of alternative mechanisms for lifting scallops out of the seabed

As the scallop dredge teeth have been identified as an important source of damage to scallops and bycatch several investigations were carried out under the Ecodredge project (Lart, ed 2003) to understand the viability of different mechanisms for lifting scallops out of the seabed. Tests were carried out on the following mechanisms.

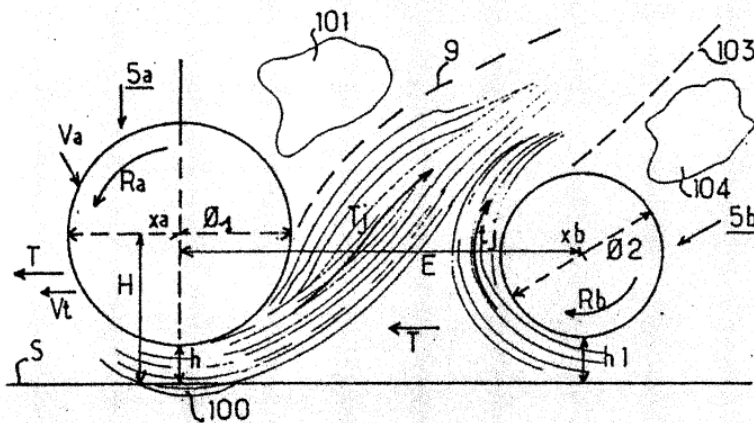
- **The Magnus** effect, which is the effect of water pressure differences around an immersed rotating cylinder. Incorporated into a dredge design using two contra rotating cylinders it has the potential for removing the scallops from the seabed via an upward flow of water between the two cylinders.

It was found possible to exploit this effect to lift scallops from the seabed using two rotating cylinders powered by hydraulics (Figure 7). However, the efficiency of the dredge was low and larger scallops were not lifted from the seabed. The necessity to supply power to the cylinders meant that the dredge was heavy and complicated.

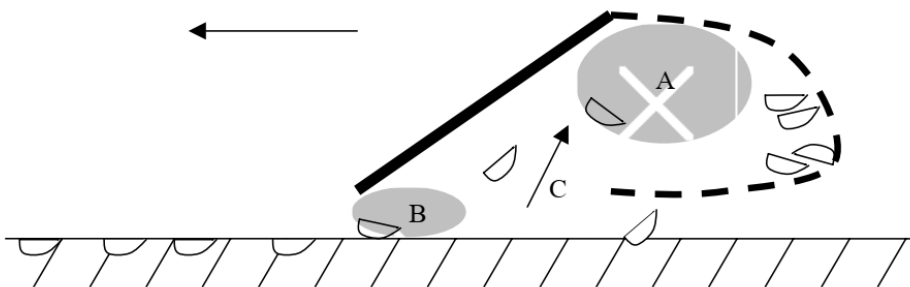
- **Hydrodynamic foils** are used to improve stability and seabed contact in certain dredge fisheries. This investigation examined whether the foil could be used to generate sufficient lift to remove scallops from the seabed. Tests were carried out using flume tank observations and computer modelling of flows around the foil (Figure 8). The study concluded that water speed under the foil is probably sufficient to remove the scallops from the seabed but insufficient to lift the scallops off the seabed and into the collector bag. There may be a role for the use of hydrodynamic effects to remove sediment from around scallops to expose them for collection and it is possible that this may already be happening in some foil dredge fisheries.
- The **Hydrodredge** (Figure 9) design is intended use hydrodynamic effects to lift the scallops into the bag with cup shaped foils set in the dredge mouth and no teeth. During trials in the scallop (*Pecten maximus*) beds around the Isle of Man in 2007 (Shepherd et al., 2008) this dredge was found to be 60-90% less efficient at catching scallops than the standard spring toothed dredge and removal of the cups had no effect on the catch of the hydro dredges. Damage rates for lethal damage (score 4) were significantly higher in the spring toothed dredges. In a further experiment (Shepherd et al., 2020) similar results were obtained in relation to damage rates, but for the single tow without cups the hydrodredge was less efficient catching only a few small scallops. Further work would be needed to fully understand this effect.

- A modified **hydraulic or water-jet dredge** with jets at varied angles to the seabed, but mostly set at  $45^\circ$  to the seabed designed to drive the scallops on the seabed surface into the collecting bag. This was tested in the French fishery in the Bay of Brest and compared with a fixed toothed French 'classical dredge' (no dive plate or sprung teeth) for capture efficiency (assessed by divers as the fraction of scallops retained by the gear compared with those left on the seabed), damage rates and length distributions. The mean capture efficiency was 13% for the hydraulic dredge and 47% for the classical dredge. Damage rates of scallops encountering the hydraulic scallop dredge (both in the catch and the seabed) were a factor of 4 lower than the classical dredge.

The hydraulic dredge in the form tested is too complex and inefficient for commercial use



**Figure 7** Functioning principle of the Magnus effect with 2 cylinders.  $R_a$  and  $R_b$ : Rotating direction,  $T$ : Translating movement relatively to the sea floor,  $V_t$ : Towing speed,  $V_a$ : Peripheral speed,  $T_j$ : Trajectory of water particles,  $h$  and  $h_1$ : Ground clearance (NB there was a patent on this dredge in 2003)



**Figure 8** Principle scheme of the foil lift effect dredge: the lack of pressure in A creates a suction in B which removes the scallops. The scallops are lifted by the foil (bold line) and collected in the basket (discontinued line).

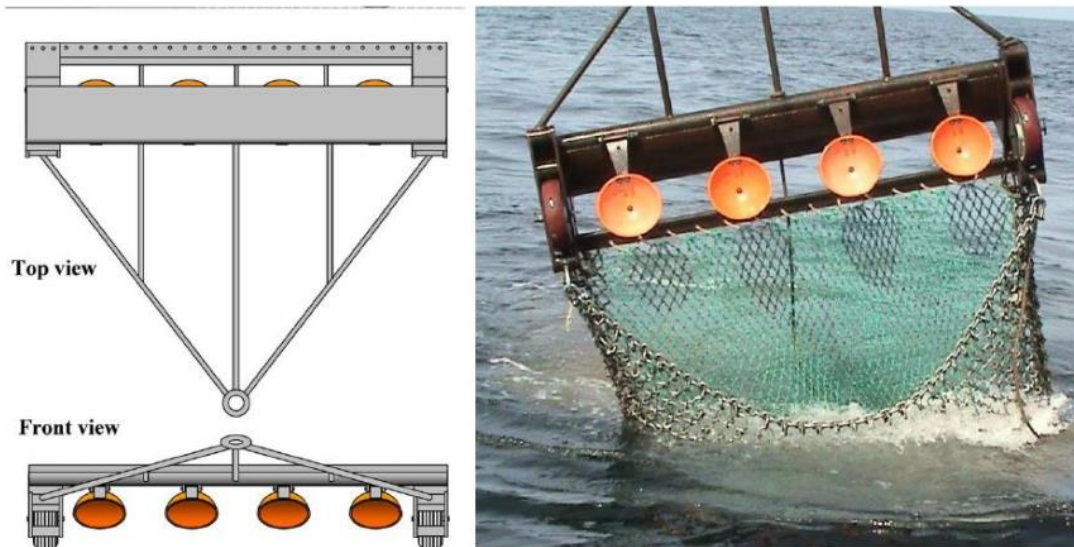


Figure 9 The Hydrodredge; the four cup shaped structures are intended to create turbulence enabling the scallops to be lifted into the bag



Figure 10 The hydraulic or water jet dredge, designed and built by IFREMER for the Ecodredge project for catching scallops. The angle of the water jets was varied, but mostly set at 45° see Lart ed., (2003)



**Figure 11** Image of dredges with (from right to left) two and three skids attached, during sea trials. Designed by Ewout Costerus (Cyclone Marine Ltd) and John Coppack (Gannet Marine Ltd). Image: Ewout Costerus.

## 2.5 Effects of changes in dredge belly design

The observation that dragging a heavy steel chain mail scallop dredge belly over the sea bed can have a serious abrasive effect on the seabed, breaking up surface dwelling biota and causing physical alteration of the seabed has led to investigations of dredge belly designs that potentially reduce this effect. Examples are;

- ‘Skid dredges’ designed by Cyclone Marine Ltd and Gannet Marine Ltd which have supportive skids shackled underneath the dredge belly. These lift the dredge belly off the seabed and so reduce the surface area in contact with the seabed (Figure 11). The extra weight of the skids can be offset by reducing the thickness of the belly rings, because the bellies are subject to less abrasion. To date, these dredges have been tested in beach trials and some limited sea trials. The beach trials indicated that although there was impact from the teeth and skids, organisms can pass under the dredge and remain intact. Initial sea trials indicated catch rates were similar to standard gear although with limited replication (Catherall and Kaiser, 2014). Further sea trials are underway (April 2021).

- Alternative materials for belly designs have been tested by Oban Scallop Gear Ltd (Figure 12) These use synthetic plastic materials instead of the hardened steel belly rings, reducing weight of the dredges. There is some evidence of reduced catches of stones. However, durability of materials is likely to be an issue (see section 4).

These results support the view that it is possible to alter the design of the dredge belly in ways which reduce its abrasion of the seabed. Altering the design may have other benefits such as reduced stone retention, seabed friction, wear on the bellies and fuel consumption.



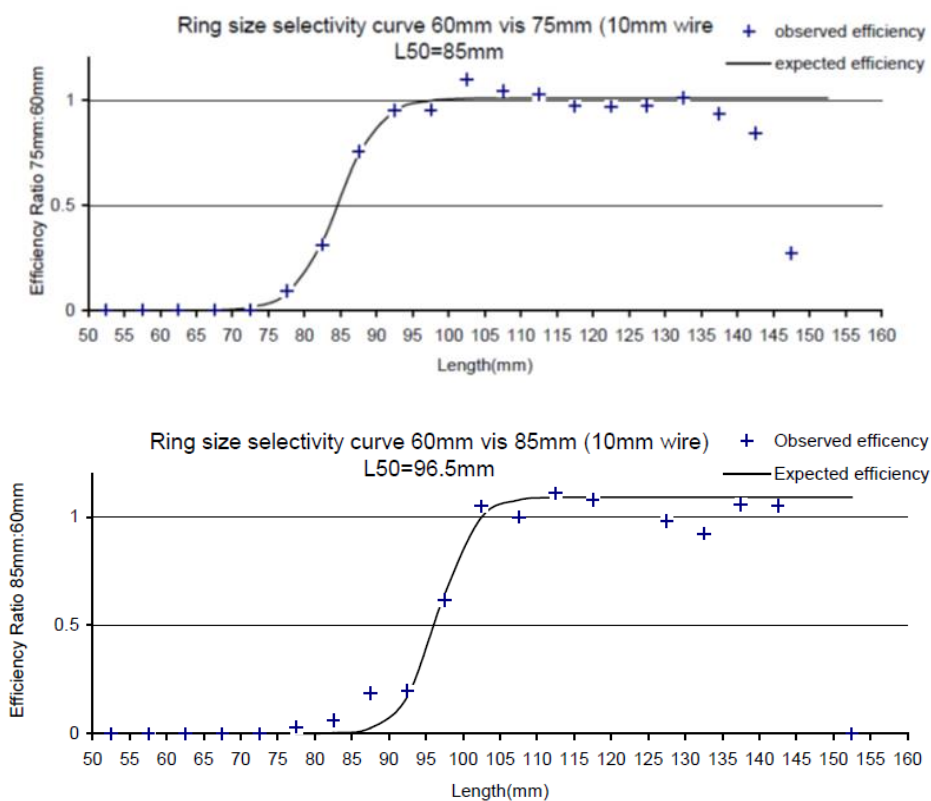
**Figure 12** Sea trials of the Oban dredge (centre two dredges) compared with standard spring toothed dredges

## 2.6 Scallop belly ring selectivity

The Ecodredge project (Lart ed., 2003) studied the effect of tooth spacing, belly ring size and mesh size of the backs of dredges (where fitted) on dredge selectivity. Of these components tooth spacing (discussed above) and ring size were found to contribute to dredge selectivity.

In UK waters the English, Northern Irish and Isle of Man technical measures result in an  $L_{50}$  of 85 mm and the Welsh measures result in an  $L_{50}$  of 97 mm (see Figure 13; note length of shell is across the flat side of the shell parallel to the hinge, the same dimension as the MCRS).

The MCRS's of 100, 105, and 110 mm (and the EU MCRS) Table 2 and Table 3 are larger than the  $L_{50}$ s and implies that there will be some discarding of undersized scallops, the amount dependent on the size distributions of the scallop populations encountered. Measures which could reduce this quantity would be increasing the belly ring size. The main benefit which would accrue from increasing selectivity of the dredges would be to reduce the time the scallops spend in the gear, hence reducing stress on the scallops as discussed in Section 2.2. However, there are issues with the durability of larger rings (see section 4).



**Figure 13 Selectivity curves and  $L_{50}$  for three internal diameters of scallop dredge belly rings using 10 mm wire. More selectivity information is available in the Ecodredge report Lart ed (2003)**

### 3 Robotic dredge designs

The advent of underwater technology used in Remotely Operated Vehicles (ROVs) has led to speculation that building an autonomous scallop harvester which is allowed to seek out and harvest scallops in a less invasive way than standard dredges may be feasible. This approach has been reviewed in [Bent et al., \(2004\)](#). A towed version, which relies on a human operator to actuate the harvesting mechanism when scallops are observed on a video link, has been



designed, built, and operated in the west of Scotland, shown in Figure 14<sup>4</sup>. This has been tested and would be considered viable at relatively high densities of scallops around 7 m<sup>2</sup>.



Figure 14 Towed scallop collector

#### 4 Materials used in dredge construction

The harsh operating conditions in the dredge fishery, most notably the severe abrasion which the dredges are subjected to in being towed across the seabed has led to investigation of wear patterns of the scallop dredge belly rings and the relative strength of different ring sizes and also the relative hardness of other materials with potential use in dredge construction.

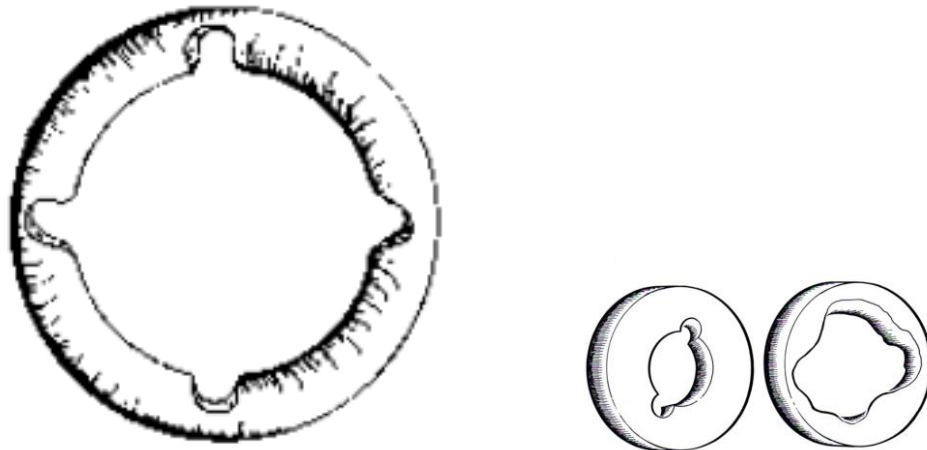
Scallop dredge belly rings are subject to point erosion, both on the rings and washers which join the rings together (Figure 15). This means that as bellies age they tend to become less efficient at retaining scallops and more prone to damage.

To understand the implications of increasing ring size to improve selectivity, the relative strength of several different sizes of new belly rings was estimated using engineering formula. The results are shown in Table 5. This table shows the tensile strength of the bellies relative to 75mm bellies based on stress calculations and allowing for the different numbers of rings across the different bellies. For new 75mm rings (10mm wire) the force required to

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<sup>4</sup> Please contact the author for further information

bend them is a load of around 200kgf per ring. This compares with the load on the dredge at the point of attachment to the bar of 100-180kgf.



**Figure 15** Left; scallop dredge belly ring with characteristic notching of point wear points, right; worn and severely worn belly ring washers

**Table 5** Relative strength of bellies (10mm wire 9 rings across) to a 75mm ring (10mm wire belly 10 rings across) based on Warnock and Benham (1965)

Ring internal diameter mm	Wire thickness	Relative Strength %
80	12	141
85	10	81
88	12	132
92	10	76

If all the tension from one dredge came on one ring (as when an obstruction was encountered) then new rings might be bent but for normal circumstances they are well in excess of requirements. Thus, the elongation of the rings is most likely a consequence of the rings losing material around the points where the washers abrade them. This will not only result in reduced thickness at this point and hence a loss of strength but also a concentration of the stress at these points in the rings. Hence avoiding the notching of the rings and washers is the key to longer lasting bellies, and improved endurance for larger belly ring sizes. Hardened steel is used to counter this abrasive effect

Abrams (2009; Appendix A) compares the properties of various possible polymer materials which might be considered for use on dredges with standard carbon steel and hardened and tempered Carbon steel. These results are shown in Table 6. The steel is characterised by increased hardness (higher Brinell hardness) indicating more resistance to abrasion and increases tensile strength than the polymers. Such information should help guide choice of materials for dredge construction

**Table 6 Material properties of two grades of carbon steel to BS specifications compared with various polymers. UTS = ultimate tensile strength. The Brinell hardness scale is a description of the resistance a material exhibits to permanent deformation by penetration of another harder material (from Abrams, 2009).**

**080M40 (EN8) BS970: 1991 (1955)**

Composition	Carbon	Manganese	Phosphorus	Sulphur
%	0.36-0.44	0.6-1	0.05 max	0.05 max

Mechanical properties	UTS N/mm <sup>2</sup>	Yield N/mm <sup>2</sup>	Elongation %	Brinell Hardness
Normalised	550	280	16	152-207
Hardened and tempered	625-775	435	12	179-229

**070M55 (EN9) BS970: 1991 (1955)**

Composition	Carbon	Manganese	Phosphorus	Sulphur
%	0.5-0.6	0.5-0.9	0.05 max	0.05 max

Mechanical properties	UTS N/mm <sup>2</sup>	Yield N/mm <sup>2</sup>	Elongation %	Brinell Hardness
Normalised	700min	355	12	201-255
Hardened and tempered	850-1000	595	9	248-302

**Polymers**

Name	UTS N/mm <sup>2</sup>	Elongation %	Shore Hardness	Brinell*** Hardness	Relative Density
HDPE	32	55	D69	50	0.94
ABS	38	20	-	-	1.04
Polycarbonate	72	100	D80	60	1.35
Nylon*	79	50	D60	46	1.15
Nylatron**	86	25	85	63	1.16
PEEK	110	20	D85	63	1.31

\*Nylon 6-6

\*\*MoS2 filled type 6/6 polyamide

\*\*\* Approximation

## 5 Conclusion; Comparison of dredge designs

The characteristics of the main dredge designs are presented in Table 7 (similar format to Catherall and Kaiser (2014))

**Table 7 Performance of alternative dredge designs compared to the standard Newhaven scallop dredge, based on current literature and research: – ✓ performs better; X performs worse; (~) equivalent performance; NA - no data available; (?) - partial evidence / inconclusive, or requires further investigation WIP= work in progress**

Gear	Impact on Seabed	Scallops retained	Stress in scallops	Bycatch retained	Fewer stones	Damage to catch & bycatch	Fuel efficiency	Notes
<b>Scallop collection methods</b>								
Increased tooth spacing where appropriate for MCRS	~	~	✓	✓	NA	NA	~	Improves selectivity and hence reduces stress in uncaught scallops
Nvirodredge™	~	~	~	~	✓	✓	✓	Possible slight increase in scallops retained
Magnus effect	NA	X	NA	NA	NA	NA	NA	Did not catch large scallops
Foil Effects	NA	NA	NA	NA	NA	NA	NA	Theoretical and flume tank study only
Hydrodredge	NA	X	NA	NA	NA	✓	NA	

Gear	Impact on Seabed	Scallops retained	Stress in scallops	Bycatch retained	Fewer stones	Damage to catch & bycatch	Fuel efficiency	Notes
Hydraulic dredge	NA	X	✓?	NA	NA	✓		Tested in comparison with French classical dredge
<b>Design of bellies</b>								
Skid dredge	✓?	~		WIP	WIP	WIP	WIP	Further trials in progress
Oban dredge	NA	~	~	~	✓	??	??	Materials durability may be an issue
Increase belly ring size	~	~	✓	✓	~	??	~	Improved scallop selectivity would reduce stress in scallops
Scallop collector	NA	See notes	NA	NA	NA	NA	NA	Requires relatively high densities of scallops around 7 m <sup>2</sup> to be viable



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## Appendix 1 AEC as a stress indicator

AEC is defined by the ratio:  $AEC = (ATP + 0.5ADP) \div (ATP + ADP + AMP)$

Where: ATP = adenosine tri-phosphate, ADP = adenosine di-phosphate and AMP = adenosine mono-phosphate.

The tri-phosphate bond of the ATP molecule has maximum energy, the di-phosphate bond of ADP is half as rich and the monophosphate bond (AMP) lacks energy. The AEC ratio ranges from 0 to 1 i.e. 0 (all nucleotides are AMP) and 1 (all nucleotides are ATP). Therefore, the level of these bonds can be used as a measure of the energy directly available to the cells at that particular time. High AEC levels (>0.8) have been found in organisms living in optimal conditions where the animals were growing and reproducing. Levels between 0.5 and 0.7 have been found in organisms whose environment was limiting in some way, such animals had reduced growth rates and did not reproduce but recovered when returned to optimal conditions. Organisms whose AEC levels were less than 0.55 had a negative scope for growth and did not recover. Scallops appear to be more tolerant of low AEC levels see Maguire et al (2002a,b)

## Appendix 2 Possible dredge design criteria

Criteria	Possible indicators
<b>Alteration of seabed habitat</b>	Reduction in catch of stones and other inorganic matter
	Reduced point loading, shearing and penetration into the sediment
	Reduced damage to seabed living (benthic) organisms
<b>Improved survival of affected organisms through; Reduction in effects on scallops</b>	
	Reduced damage rates
	Improved size selectivity
<b>Reduction in effects on non target organisms</b>	
	Improved species selectivity
	Improved survival of bycatch species such as crabs
	Improved survival of other organisms encountered on the seabed
<b>Commercial viability</b>	
	Catching efficiency maintained
	Handling and safety improved or maintained
	Fuel consumption maintained or reduced
<b>Legislative</b>	
	UK legislation in force specifies dredges with a certain level of species and scallop size selectivity. Innovative dredges would have to meet or improve on these standards.



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